BAM Gold Project – January 2019 MRE

Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.*	• Sampling techniques are described for the drilling programs for the BAM Gold Project conducted by Landore Resources Canada Inc. ("**LND**") from December 2015 up to September 2018. • Surface diamond drill ("**DD**") core sampling is the main sample type. • Extracted core was placed in a core cradle, ensuring that core was maintained intact and in the correct order. Core was cleaned with segments pieced back together in order to reconstruct the in-situ position as closely as possible. • Core was placed into numbered wooden core boxes in which the regular wooden blocks were inserted with drilling depth labelled on the blocks, then had lids fixed to the top of the trays to minimise disruption of the core during transportation back to the core shack at LND's Junior Lake exploration camp. • Some channel sampling from trenches cut at several exposed outcrops has been carried out previously. Channel samples were used to prepare the lithologic interpretations and preliminary outlines of the extent of the gold mineralization.
	• *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.*	• Two sizes of diamond drill core are used - NQ and HQ (+HQ3) diameter. The NQ size is used primarily for exploration drilling and for some drilling in the main mineralisation zone. The larger HQ size is used within the central mineralisation zone of the BAM area to obtain a larger representative sample. • All DD Core was geologically logged and sampled to lithological contacts or changes in the nature of mineralisation to ensure a sample representation of lithological/alteration/mineralisation intervals. • Sample intervals are typically 1.0m to 1.5m in length. For sampling completed to September 2018, minimum sample length was 0.18m, and maximum length was 2.2m.
	• *Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.*	• Industry standard core sampling procedures were employed: 1. All drill core is aligned and measured prior to sampling: 2. Samples for assay are selected and marked for sampling on the basis of sulphide geology/mineralogy and rock units; 3. Sample intervals avoid crossing geological contacts; 4. Samples are sawn in half with a diamond saw blade; 5. One half of the sample is placed in a standard, numbered transparent plastic bag with an identifying sample tag and - the remaining half returned to the core box with a corresponding tag placed at the beginning of the sample interval; 6. The halved drill core is retained in core racks on site. • DD core was used to obtain representative half core samples weighing 3kg to 5kg, which was

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		sufficient to be pulverised to produce a 50g charge for fire assay.
Drilling techniques	• *Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	• Drilling techniques are described for the drilling programs for the BAM Gold Project conducted by LND from December 2015 up to September 2018. • The 2015-2087 drilling campaigns were conducted by Chibougamau Diamond Drilling, of Chibougamau, Québec. • All holes were entirely drilled by surface DD core drilling, either NQ or HQ diameter, with a 3m core barrel and standard inner tube. DD core was not oriented.
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.*	• For DD core, core recovery length and percentage of both the total drilled interval and for each metre interval was calculated and recorded. • The longest and smallest pieces of drill core in the three metre intervals were measured and recorded, as well as the fracture density. The fracture density is the visual inspection of the intensity of natural fractures in a given three metres and is a numerical value on a scale of 0 to 9 (0 being no fractures, 9 being very intensely fractured). • Core recovery is reported as a percentage of the drilling interval and calculated using the following formula: • **Core recovery = (Metres recovered/metres drilled) *100** • LND has reported that core recoveries are typically >95% except in rare cases over narrow intervals of highly sheared, foliated intervals. As such it is considered that samples accurately reflect drilled widths sampled.
	• *Measures taken to maximise sample recovery and ensure representative nature of the samples.*	• All DD core was either NQ or HQ diameter and utilized a 3m core barrel to maximize recovery and to provide a representative sample.
	• *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	• An analysis of DD core recovery relationship with grade and sample bias has been conducted for DD core from 2015 to 2018, which encompasses all of the BAM Project area drilled to date. • Overall the core recovery is excellent for all DD holes where core recovery % has been recorded since 2015 for the BAM project. • A review of the core photos from the 3m core runs where core recovery is recorded as <90%, clearly indicate small intervals (0.5m to1.0m) within the core run where there is core loss and poor quality, highly fractured core. • There is evidence that a sample bias occurs where there is poor recovery, resulting in lower Au values. This is demonstrated by the twin hole analysis for holes 0418-632 vs 0418-676. • However, the data population for poor recovery holes is very small, so it may not be correct to assume this is the case in all occurrences where poor recovery has occurred. • In summary, there does not appear to be sufficient evidence to suggest the small poor core recovery intervals in the selected holes would impact significantly on the resource grade

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		estimates within the interpreted mineralisation envelopes reviewed in this analysis.
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.*	• All DD core was aligned, measured and logged at in the LND Junior Lake exploration camp site, with additional logging and sampling of mineralized core in the LND warehouse in Thunder Bay. • Geotechnical measurements including core recovery, rock quality designation ("**RQD**"), and fracture density were also taken. • Logging records major and minor rock units (grain sizes, texture structural information: core angles of geological contacts, foliation and bedding, fractures, faults, veins, joints etc.), alteration and sulphide species, content and mode of occurrence. • Logging and sampling information was recorded by hand on paper and/or in MS Word and MS Excel software, and then edited as required. • MS Access and MapInfo GIS databases are maintained for all drilling information available for Mineral Resource estimation ("**MRE**") work, and mining and metallurgical studies.
	• *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.*	• Logging has predominantly been conducted both qualitatively and quantitatively with description of lithologies, structural measurements and comments being done. • All DD Core is digitally photographed for both dry and wet core trays with photos maintained on file in LND's Thunder Bay office.
	• *The total length and percentage of the relevant intersections logged.*	• The lithology tables show 9,506 lithology entries for 31,594m of all drilling completed on the Project up to December 2018 and relevant to the current MRE. • The total drill metres recorded in the collar records is 20,309.8m, which shows that 100% of the drill metres within the drill hole database have been logged.
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.*	• All DD Core to date has been half core sampled.
	• *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.*	• Not applicable, as only DD core sampling has been carried out.
	• *For all sample types, the nature, quality and appropriateness of the sample preparation technique.*	• Conventional core sampling procedures were employed. All DD core was aligned and measured prior to sampling. Samples for assay were selected and marked for sampling on the basis of sulphide geology/mineralogy and rock units. Sample intervals avoided crossing geological contacts except for a few instances. • For all recent drilling programs, the core was cut in half using a Vancon diamond saw. One half of the sample was placed in a standard, numbered transparent plastic bags with an identifying sample tag and the remaining half returned to the core box with a corresponding tag placed at the beginning of the sample interval. This drill core is retained in core racks on site. • Core samples were transported directly from the site to the ALS Chemex ("**ALS**)" preparation facilities in Thunder Bay, Ontario, by LND personnel. 1. The sample preparation procedures used by ALS were as follows:

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		2. The rock samples were first entered into the ALS Local Information System ("**LIMS**"), then bar-coded and weighed. 3. The samples were dried, riffled split, and then crushed?) to better than 70% -2 mm. Silica sand was used to clean out the pulverizing dishes between each sample to prevent cross contamination. 4. The homogeneous sample then received final preparation and was analysed as per the required methods. • The nature, quality and appropriateness of the sample preparation protocols is considered appropriate for grain sizes of the material expected and is consistent with industry standard practice.
	• *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.*	• Quality Control procedures used during the sub-sampling preparation include: o Tracking to avoid sample swapping or other preparation errors - The rock samples are entered into LIMS, then bar-coded; o All samples are weighed; o Silica sand is used to clean out the pulverizing dishes between each sample to prevent cross contamination; o It is not recorded whether the laboratory carries out homogeneity checks (grind size checks).
	• *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.*	• LND re-submitted a total of 373 pulp samples and 272 pulp reject samples derived from the DD core drilled from 2015 to 2017 to ALS for screen metallic gold analysis (analysis code Au-SCR24) to check reproducibility of gold assays for (ALS), and for check assaying of the primary lab results by an umpire laboratory (Accurassay of Thunder Bay, Ontario, "**Accurassay**"). • This analytical method consists of passing the pulp sample through a (-) 100 micron screen and analysing the resultant sample portions using fire assay with AA finish (ALS analytical code Au-AA26). • No RC or other drill chip sampling completed, so there are no field duplicates. No second half or quarter core samples are known to have been taken to date.
	• *Whether sample sizes are appropriate to the grain size of the material being sampled.*	• Samples delivered to the laboratory weighed in the range of 3-5kg. This is appropriate for the grain size of material for gold sampling.
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.*	• ALS has been LND's primary independent laboratory since 2012. • The majority of drill core samples from all DD drilling consisted of Au analyses by '"ore" grade fire assay with AA finish (50g) (ALS analysis code Au-AA26). • This analytical method is accredited under ISO/IEC 17025. Samples which exceed analysis Au-AA26's limit of 100g/t Au are re-analysed using fire assay with gravimetric finish (50g) (ALS analysis code Au-GRA22). • Drill holes 0415-517, 0415-518, and 0415-519 to 0415-523 were analysed for Au, Pt, and Pd using

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		fire assay with ICP-AES finish (ALS analysis code PGM-ICP23). • All drill core samples from 2015 to 2018 drilling campaigns were analysed for multi-element (35) suite by ICP (ALS analysis code ME-ICP41). • The appropriateness of the assaying and laboratory methods is considered a total measure of gold.
	• *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.*	• Magnetic Susceptibility ("**MS**") measurements were taken utilizing a Kappameter, model KP-6 magnetic susceptibility metre. • MS was measured where there was visible mineralization, and at 3m intervals in select holes for background measurements. • The measurements were entered into an Excel spreadsheet either directly or after they had been recorded by hand on paper.
	• *Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.*	• LND QAQC protocol was for sample blanks and certified reference material (standards or "**CRM**") to be inserted into the sample stream at regular intervals. Systematic check analyses on pulps (every 10th sample) were completed by ALS in Vancouver or Accurassay of Thunder Bay, Ontario. • Current LND practice for gold analyses is to insert: • 1. One gold reference standard following every 20th drill core sample; and • 2. One blank following each base element standard. • In addition, approximately five percent of the pulp and reject samples were check assayed at the secondary laboratory (Accurassay). • LND used silica sand, commercially available from mineral laboratories, for blank samples. LND has used an assortment of CRMs at various gold grades that have been purchased from WCM Minerals, Burnaby, British Columbia; Geostats Pty Ltd, Fremantle, Australia; and CANMET, Ottawa, Ontario. CRMs in 2006 and earlier were obtained from Gannet Holdings Pty Ltd of Perth, Australia. • **Results of Cube Analysis:** • The result of the gold analyses on pulp duplicate samples between ALS and the umpire laboratory (Accurassay) showed the duplicate samples for both laboratories had an average coefficient of variation ("**ACV**") which is high for the range for duplicates of the sample type (Pulp 10-20% or Reject 20-30%). The results are indicative of the "nuggety" nature of the gold mineralisation at BAM, where up to 1mm visible gold specks have been regularly logged in the DD core. • CRMs have an insertion rate of 7% and 11% insertion rate for blanks. This is adequate coverage for the drilling completed to date. • CRMs and blanks inserted in batches at ALS during the period 2015 to 2018 have in the most part, performing well. • Based on the results received from the 2015 to 2018 data which show acceptable levels of accuracy and precision, Cube is satisfied that the assay database is suitable for use in MRE work.

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Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.*	• Original laboratory assay certificates were reviewed and validated by the Cube for selected verification holes. Significant intersections were assessed against DD core on site, and with drilling logs and core photos by Cube. No material discrepancies were found. • No independent sampling has been undertaken by Cube.
	• *The use of twinned holes.*	• One DD hole has been twinned has occurred at the BAM Gold Project to date (original hole: 0418-632, twin hole: 0418-676). • The original hole displayed poor sample quality and poor recovery within a mineralised interval, and the second hole was drilled at the same location. • The twin hole mineralised zone intersection length was similar to the original hole but the grade variance was significantly higher within the twin hole. • Probable causes for the grade variance are - Poorer core recovery or possible core loss due to mishandling for original hole; Sample size is larger for twin hole (HQ core) compared to NQ core size for the original hole; Gold occurrence is very "nuggety" as evident from numerous core samples containing visible gold.
	• *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.*	• A review of the sample collection, submission, and data entry protocols was completed during the site visit to the Junior Lake exploration camp office as part of the data verification process by Cube from 23rd to 28th June 2018. • All documentation relating to drilling and sampling is collated and validated either on site or at the LND offices in Thunder Bay. Drill hole and assay data is entered or imported into LND's MS Access database. • Core logging was recorded by hand on paper in standard logging sheets, entered in MS Word/Excel software, and then edited as required. • All data is checked by the software validation and Senior Geologist for data entry errors. • In Cube's opinion, the drilling, logging, and sampling procedures at the BAM Project have been carried out to industry best practices.
	• *Discuss any adjustment to assay data.*	• The primary returned assay result was used for reporting of all intersections and in MRE. No averaging with laboratory repeats was undertaken so as not to introduce volume bias. • All assay data within the BAM MRE area below detection limit (-1) values (7,373 samples) have been entered as a small value of 0.005ppm Au which is half the lowest common value reported in the primary Au ppb analysis (10ppb Au). • The other negative values recorded, -5 (61 samples) and -7 (7 samples), are assumed to be missing samples or samples with insufficient sample weight for analysis, and were assigned as "null" values.
Location of data	• *Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine*	• Drill collars for all drilling programs were surveyed by an Ontario Land Surveyor (J. Barnes and Associates of Thunder Bay, Ontario).

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points	*workings and other locations used in Mineral Resource estimation.*	• All collars were pegged prior to the commencement of the program using a differential GPS (Trimble GPS, with accuracy +/120cm). • After the drilling programs were finished, certified contract surveyors (JD Barnes & Associates of Thunder Bay) would pick up the actual collar locations using a differential GPS or total station Electronic Distance Measuring ("**EDM**") survey equipment. • 169 DD holes were used for MRE. All of the holes have Easting, Northing and RL collar coordinates which have 2 decimal place values. This indicates all the holes are likely to have collar coordinates which actually surveyed. • Several verification holes were checked by Cube against the hole ID in the BAM MRE database. There were no variances from the original database co-ordinate records for the holes identified. • Downhole surveys were conducted at 9m depth after hole collaring and then at 50m intervals using a Reflex Easy-Shot, single-shot survey tool supplied by the drilling company. • On completion of each hole, downhole surveys were completed using a continuous Reflex Maxibor survey unit by third party contractors, providing a dip and azimuth reading at 3m intervals down hole. • A topographic surface created in 2018 in DXF file format was imported into Surpac as a DTM file for use in the MRE work. • The 3D location of the individual samples is considered to be adequately for the MRE.
	• *Specification of the grid system used.*	• The drilling completed was carried out in the UTM NAD83, Zone 16 grid coordinate system. • The drill holes are initially located within an old local grid system that was established by previous owners of the property. LND successfully located this previous grid and refurbished it for its own use. This local grid uses a baseline azimuth of approximately 087°. • The local grid system has been used to as the reference lines for the drilling fences for all of the BAM drilling programs overlain on the UTM NAD83, Zone 16 grid coordinates. • All drilling and block model data used for the January 2019 MRE work has used the UTM NAD83, Zone 16 grid coordinate system.
	• *Quality and adequacy of topographic control.*	• Topographic control of prospects in the Junior Lake property was surveyed by an Ontario Land Surveyor (J. Barnes and Associates of Thunder Bay, Ontario). • A surface topography digital terrain model ("**DTM**") file was created by LND covering the entire BAM Project area. • This file was used for validation the RLs of the hole collars derived from the surveyed collar records in the database files received from LND. • The topographic control is adequate for coverage of the BAM Project area.
Data spacing and	• *Data spacing for reporting of Exploration Results.*	• Drill data spacing is appropriate for reporting of Exploration Results and for the infill resource definition drilling programs.

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distribution		• The majority of drilling is 50m x 50m or 100m x 50m on a local mine grid north-south sections. The old local grid is 003° west of the UTM grid north. All drilling was carried out from surface.
	• *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.*	• The drilling data spacing is adequate to determine the geological and grade continuity for reporting of Mineral Resources and Mineral Reserves.
	• *Whether sample compositing has been applied.*	• No sample compositing of DD core samples has been applied for the DD drilling programs.
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.*	• Most drilling has been designed to be orientated normal to the dip of the major mineralisation zones. • Several holes were drilled to the local grid south in order to where there are access restrictions due to a dried up lake in the central area of BAM East (Ladle Flats). • The capability of drilling with shallower angled holes has provided a representative sample across the mineralisation.
	• *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	• DD holes were mostly oriented to the old local grid north (357°), with collar angles mostly drilled at -45° dip, with average depth of approximately 187m. • Mineralised structures appear to strike at approximately 280° and are steeply dipping to the south (-65 to -80° dips). Drill orientation for nearly all holes has not introduced any material sampling bias. • The results from three holes drilled to the south at shallower angles were not used in the MRE.
Sample security	• *The measures taken to ensure sample security.*	• All core sample bags are sealed with plastic sequentially numbered security tags and three to five of these sample bags are placed in larger rice bags also sealed with a numbered security tag. All security tag numbers are recorded prior to shipping and checked upon delivery at the lab. • Core samples are secured in the logging/sampling building at the Junior Lake exploration camp on site. The samples are then transported directly from the site to the Accurassay or ALS Chemex lab in Thunder Bay by LND or Chibougamau Diamond Drilling personnel. There have been no samples lost and no indications of sample tampering. • Samples were submitted in batches of 50, soon after they were collected. • Chain of custody is supported by the LND site staff sample logbook and sample reports from the laboratories.
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	• Descriptions of sampling methods and data control, including site inspections, been undertaken by LND, Cube and previous independent consultants and recorded in recent reports from 2015 to 2017. • The sampling procedures and drilling data were reviewed and audited by Brian Fitzpatrick (Cube

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		Consulting, Principal Geologist) while onsite from 23rd to 28th June 2018. • The site visit involved inspection of the drilling in progress, and onsite sample preparation facilities. • Cube conducted a data compilation review and validation of all drilling data prior to the MRE work in 2018. This involved checks of collar locations, downhole survey errors, assays and geological data – missing data, overlapping intervals, and gaps between intervals. • There were no adverse material results from any of the reviews or audits and the data is considered suitable for MRE work. • A desktop review of the QAQC results by Cube has noted the following points for further review: o Duplicate Sampling - Further analysis of the duplicate sampling is required, including the following recommendations – re-analysis of duplicate sample pulps where ACVs are high; include CRM and blanks within the duplicate sampling lab jobs; carry out coarse reject duplicate sampling. o Coarse reject samples should be retained for all batches. These are ideally suitable as a duplicate for DDH ½ core samples and could be carried out on the mineralised threshold of Au >0.10ppm including CRMs and coarse blanks throughout. o Pulp grind checks could be introduced for 1 in 20 samples per lab job to monitor sample preparation and compliance with the assay contract. o A basic QAQC check (CRM precision check) should be carried out on each batch individually upon receipt from the laboratory to determine and address any laboratory issues as they arise. If 3 or more CRMs within a batch fail, the batch should be re-analysed in full. o For future drilling campaigns, it is recommended that a smaller selection of CRMs be used, in order to have a more meaningful number of results for analysis.

Section 2 Reporting of Exploration Results

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.*	• The Junior Lake Project which includes the BAM Gold Project is located approximately 235km north-northeast of Thunder Bay, Ontario, and approximately 75km east-northeast of the village of Armstrong. • LND's mineral holdings in the Armstrong area comprise the Junior Lake claim group (100% ownership) and the immediately adjacent claim group of Lamaune Iron Inc. (Lamaune Iron). In October 2017, LND acquired a 90.2% ownership of Lamaune Iron, which has become a subsidiary company of LND. Together, the two groups consist of 113 staked mineral claims (1,429 units, 22,864ha), two patented claims, and three mining leases, all together totalling 26,59 ha. • LND's interest in the Lamaune Iron claims is subject to a 2% NSR royalty. LND is entitled, at its sole option and at any time, to buy back 1% of the NSR royalty for USD $1M. • LND has access to all of the mining and surface rights for those leases and patented claims over an area encompassing the BAM Gold Project area. The Project lies on mining lease CLM 461. • Within the mining leases, LND has the right, subject to provisions of certain Acts and reservations, to: 1. Sink shafts, excavations, etc., for mining purposes; 2. Construct dams, reservoirs, railways, etc., as needed; and 3. Erect buildings, machinery, furnaces, etc., as required, and treat ores. • LND has recently reported that there are no environmental liabilities associated with the Junior Lake properties.
	• *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	• LND has recently reported that there are no other significant factors or risks that may affect access, title, or the right or ability to perform the proposed work program on the property.
Exploration done by other parties	• *Acknowledgment and appraisal of exploration by other parties.*	• <u>SUMMARY OF EXPLORATION WORK by LANDORE:</u> • LND optioned part of the Junior Lake property from North Coldstream Mines Limited in 1998 and additional claims from Brancote Canada in 2000. Since then, LND has found nine PGE-Cu-Ni occurrences, one Cu-Pd zone, two gold zones, and Zn-Au-Ag and Zn-Co occurrences in old trenches and boulders bearing base and precious metals or arsenic mineralization. • LND has successfully delineated several deposits and other potential areas of significant mineralization throughout the Junior Lake property including the BAM East Gold Project, the Lamaune Gold Project, the B4-7 Ni-Cu-Co-PGE Project, and VW Ni Project.
Geology	• *Deposit type, geological setting and style of mineralisation.*	• **REGIONAL GEOLOGY** • The Junior Lake property is located within the Archean-aged Superior Province of the Precambrian Shield which hosts most major mining camps in Canada in the core of the North American continent. The Superior Province is further subdivided into numerous provinces of varying aged tectonostratigraphic, plutonic, and supracrustal rock assemblages. The Junior Lake

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		property is located within the East Wabigoon Sub-province. The property is within the roughly east-west trending Caribou (Lake)-O'Sullivan greenstone belt. This greenstone belt ranges from 3.5km to 15km wide and extends roughly east-west for 80km to 100km (MacDonald, 2006). The belt is flanked to the south by the Robinson Lake Batholith portion of the Lamaune Batholithic Complex and to the north by a major, roughly east-west trending fault zone that marks the southern boundary of the English River Sub-province. Northeast of the property, the belt is intruded by the Summit Lake Batholith which is of tonalitic to quartz dioritic composition. The western portion of the greenstone belt has been intruded by thick, undulating, flat-lying, Neoproterozoic-age Nipigon diabase sills and cross-cutting dikes. These sills are thought to represent the discontinuous, erosional remnants of thick, laterally extensive sills comprising the Nipigon Plate, which is centred on Lake Nipigon, approximately 30km to the south. The Junior Lake property is located within the boundaries of the geologic map of the Crescent Lake area by Pye (1968). The property is host to the BAM East Gold Project located approximately midway between the B4-7 Ni-Cu-Co-PGE deposit and the VW nickel deposit, located three kilometres apart. The BAM gold outcrop is approximately one kilometre west of the BAM East Gold Project. • **PROSPECT GEOLOGY & MINERALISATION** • The BAM Gold Project is located in the south central area of the Junior Lake property and is interpreted as an Archean-aged mesothermal gold deposit. The deposit consists of gold mineralization that is hosted by sheared and altered rocks of the Grassy Pond Sill and the BAM Sequence. The deposit has been traced by detailed drilling at approximately 50m centres along a strike length of approximately 1,000m. Reconnaissance-scale step-out drilling has also intersected gold mineralization in the same host rocks along a strike length of approximately 1,900m. Based upon the information collected from the detailed scale diamond drill holes, the host rock units strike in an east-southeast direction and dip steeply to moderately to the south at 65° to 80°. The gold mineralization is interpreted to reside within a series of tabular shaped zones that are oriented in a roughly en-echelon configuration and are generally parallel to the overall strike of the host rock units. • The gold mineralization is commonly observed in drill core to exist as visible gold that is hosted by very thin, foliation-parallel quartz-rich veinlets, hosted by highly fissile ultramafic sediments of the BAM Sequence, or by foliated rocks of the Grassy Pond Sill. A preliminary petrographic study carried out on a number of samples has identified the presence of coarse native gold that is present in association with either tourmaline, ankerite, or scheelite assemblages that occur within calcite replacement patches and veinlets.
Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:*	• A summary of all drilling completed by LND during 2018 are shown Appendix A. • Reporting of exploration results relating to the BAM Project up to September 2017 have been previously reported by LND in the December 2017 - *LANDORE RESOURCES LIMITED (AIM Ticker: LND.L) UPDATED MINERAL RESOURCE ESTIMATE BAM EAST GOLD DEPOSIT, JUNIOR LAKE*

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	○ *easting and northing of the drill hole collar* ○ *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* ○ *dip and azimuth of the hole* ○ *down hole length and interception depth* ○ *hole length.*	*PROPERTY. RNS Number 8938Y, 11th December 2017*. • The co-ordinates for Easting, Northing and RL of the hole collars are recorded in UTM NAD83, Zone 16 grid coordinate system. • Dip is the inclination of the hole from the horizontal. For example, a vertically down drilled hole from the surface is -90°. Azimuth is reported in magnetic degrees as the direction toward which the hole is drilled. • Downhole length of the hole is the distance from the surface to the end of the hole, as measured along the drill trace. Interception depth is the distance down the hole as measured along the drill trace. Intersection width is the downhole distance of an intersection as measured along the drill trace
	• *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	• It is the opinion of the competent person that the exclusion of the drilling data in the Table 1 does not detract from the understanding of the report, as all information has been previously reported.
Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.*	• Diamond core was cut to geological boundaries, so length weighting was used in the reporting of exploration results to ensure a logical mean grade is determined. • No grade truncation or high grade cutting was applied in the results reported in December 2017.
	• *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.*	• The co-ordinates for Easting and Northing of the hole collars for significant intercepts reported are recorded in the both the UTM NAD83, Zone 16 grid coordinate system and the local grid co-ordinates in the results reported as reported by LND during 201. • The start of the downhole intercept, and the downhole length are reported. • Holes 0417-619 and 0417-624 were drilled at 40° with all others at 45 ° into a lithological package dipping approximately 40° to the south. The actual true thickness of mineralisation is estimated to represent between 85% and 90% of the intervals shown in the above table.
	• *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	• Metal equivalent values have not been used. Only gold grade is reported.
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.*	• Drilling orientations have been designed to intersect the mineralisation orthogonal to dip and strike. The drilling orientations are occasionally compromised by a small lake/mud flats on the surface.
	• *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.*	• Geometry and true widths of the mineralisation zones within the BAM Gold Project are well understood because the area has been infill drilled on a regular spacing using only DD core since the 2015.

Criteria	JORC Code explanation	Commentary
		• This information has been used to create 3D models of the lithologies and mineralisation domains. It is well known that the main mineralisation zones dip steeply toward 280^{O} at -65 ^{O} to -80^{O}.
	• *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').*	• Infill drilling has provided sufficient confidence in the current mineralisation true widths for the main mineralisation zones in the BAM Project area.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	• A drill hole location plan showing recent drilling stages, and representative drill section are illustrated Appendix B.
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	• Significant results from the 2018 DD drilling program that relate to the BAM Gold Project have been reported in Appendix A.
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	• No other exploration data is reported as part of this release.
Further work	• *The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).*	• The 2018 DD program aimed at testing infill and down dip extensions to known mineralisation that is not closed off and step out drilling to the west of the main mineralisation zones at BAM East. This program was completed in September 2018. • Future drill testing recommended to target gold mineralisation still open along strike and down dip is listed as follows: 1. Infill drilling within and below December 2018 Pit Design – enable confidence in grade continuity along strike;

Criteria	JORC Code explanation	Commentary
		2. Infill drilling and Step out drilling to target strike extensions of the main BAM hosted Au mineralisation – enable potential upgrades of Inferred to Indicated, and potential conversion of Unclassified material to Mineral Resources; 3. Highly prospective IP Anomaly targets have been identified by LND previously in 2006 and related to FW massive to disseminated sulphides zones within the main BAM Au mineralised units. In addition there are 3 to 4 WNW trending anomalies that are possible targets for exploration drilling (northern anomalies), and step-out drilling along strike from the BAM sequence. 4. Regional Prospectivity – other gold mineralisation targets along the 31km strike length of the Junior Lake Shear (Lamaune) and historic discovery at Toronto Lake.
	• *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	• Relevant location plans showing potential extensions to mineralisation illustrated in Appendix C.

Section 3 Estimation and Reporting of Mineral Resources

Criteria	JORC Code explanation	Commentary
Database integrity	• *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.*	• Cube compiled the electronic data received from LND for importing into a MS Access format database. This database has been relied upon as the source of data for the January 2019 MRE work completed by Cube. • Collar, survey, assay, geology and other relevant drilling data were extracted by LND in November as ASCII file format (*.txt) and MS Excel file format (*.xlsx) for use in the January 2019 MRE. Cube validated the data prior to importing into a Cube standard and structured MS Access database which was then mapped into Surpac v6.8.0.
	• *Data validation procedures used.*	• Cube completed validation checks on the database comparing collar points to the topography, maximum Hole depth checks between tables and the collar data, duplicate numbering, missing data, and interval error checks using validation rules in MS Excel before importing records into MS Access. Cube then verified the data using visual inspection of the holes in Surpac v6.8 and Leapfrog Geo v4.2 to check hole collar positions in relation to topography, and identify any inconsistencies of hole traces. • The trench sampling results were not used in the 2018 MRE. • A validated assay field was included into the Assay table (au_use) to convert any intercepts that have negative values or blanks in the primary Au field (Au_ppb FA50). • All -1 assay values were set to 0.005g/t Au and all un-sampled locations were assumed to be waste and were given a background grade 0.005g/t Au grade for the estimation process. • The other negative values recorded, -5 (61 samples) and -7 (7 samples), are assumed to be missing samples or samples with insufficient sample weight for analysis and were assigned as “null” values and ignored when extracting composites for grade interpolation.
Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.*	• Brian Fitzpatrick (Principal Consultant – Cube Consulting) who is the Competent Person conducted a site visit from 23rd to 28th June 2018. Field notes and photographs were taken along with discussions with site personnel regarding geology and mineralisation of the BAM Project, sampling and QAQC protocols. • The 2018 site visit by Cube included the following activities: o The site visit included inspection of current DD drilling and sampling activities and facilities, and inspection of the sample despatch and security at the site sampling and storage facilities; o Examination of DD core and core logging activities on site – geological and geotechnical and carried out discussions with the on-site geologists regarding the current understanding of the nature of the host rocks and controls on the gold mineralization; o Inspection of diamond drill rig and drilling activities; o Inspection of outcrops, inspected the general topographic conditions in the area of the Project; o Identifying location of a number of surface drill hole collars; o The lithologies, structure, alteration, and mineralization in selected intervals of drill core were

Criteria	JORC Code explanation	Commentary
		examined and compared with the descriptions presented in the drill hole logs. No material discrepancies were noted.
	• *If no site visits have been undertaken indicate why this is the case.*	• Not applicable.
Geological Interpretation	• *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.*	• The confidence in the geological interpretation of the January 2019 MRE is good as a result of the optimally spaced DD drilling programs, predominantly between 2015 and 2018 by LND. • Geological and mineralisation interpretations in plan and cross sections have been followed up with 3D wireframe models based on analysis of all the recent information collated.
	• *Nature of the data used and of any assumptions made.*	• Data is sourced from the recent hard copy cross section and plan interpretations based on drill logging and sampling. The logging information has been used by LND to interpret stratigraphic units, major structural features (dyke intrusives, major faults) and mineralisation trends. • An overburden surface DTM was interpreted for a 10-15m thick glacial till which acted as a boundary with the interpreted lithological units and mineralisation domains underneath. • Plan view slices were used to interpret lithology and potential fault offsets. • Cube interpretation contained broad zonation of the main BAM Sequence mineralisation. • Mineralisation domain projections were made between drill sections and extending along strike and down dip based on a consistent drill spacing of 50m x 50m. • Interpretation of the main BAM mineralisation was projected further along strike and down dip for conceptual modelling and potential drill targeting within the BAM sequence. • 3D wireframing of the lithological units and overburden surface allowed for assignment of the density values for the mineral resource estimate.
	• *The effect, if any, of alternative interpretations on Mineral Resource estimation.*	• The one major change compared to previous interpretations has been the broadening of the main BAM mineralisation domain (Domain 1001). Previous interpretations included very narrow domaining of high grade zonations within the BAM Sequence. Many of these sub-domains were in close proximity and were not consistent in orientation and true thickness from one section to the next. With the likelihood of open pit mining methods, broader domaining with minimum open pit mining SMU width was used as a guide for updated interpretation.
	• *The use of geology in guiding and controlling Mineral Resource estimation.*	• The interpretation of the mineralisation domain boundaries was guided by the orientation of the main lithological units in 3D and from observations noted from LND hard copy sections, and observations from DD core viewed on site • Descriptions of alteration, mineral assemblages and grade distribution within each host lithological units were also used to inform mineralisation domain boundaries. • The main BAM mineralisation was guided by the Hanging wall (HW) contact with the Grassy Pond Sill unit (gabbro). Mineralisation often crosses the HW contact, so there is not a consistent

Criteria	JORC Code explanation	Commentary
		boundary directly on the contact. Within the BAM sequence, the main mineralisation grade varies, as evident from the visible gold observed in DD core. In some sections, the domain interpretations were drawn to include intervals in the drill holes where the average grades did not meet the nominal cut-off grade criteria (0.2g/t Au) as identified from the Domain boundary analysis. • Minor mineralisation domains occur along the BAM sequence footwall (FW) contact and also within sheared and altered "lensoidal" zones within the hanging wall sequence. Gold mineralisation tends to be less continuous and narrower outside of the main BAM Sequence host unit.
	• *The factors affecting continuity both of grade and geology.*	• Grade distribution plots were created in Surpac to assist with assessing grade continuity along strike, down dip, and to assess if any down plunge component was apparent. Domain 1001 displayed good anomalous Au continuity along strike for ~600m with an apparent WSW plunge component of ~16^{o}. There is also an apparent offset at Line 2800E that has been conceptually interpreted and is possibly a significant fault structure. Both interpretations require further drill testing and assessment with more information at hand. • All mineralisation domain outlines were modelled to a nominal grade cut-off of approximately 0.2g/t Au cut-off which allowed the model shapes to have optimum continuity. • The use of this low grade threshold has resulted in some areas having simplified mineralised domains encompassing discontinuous tabular shapes. • The main BAM mineralisation is steeply south dipping which narrows to both the west and east, although drill lines 200m away in both directions have intersected significant mineralisation along the general strike of the main anomalous trend. • LND sectional interpretations show apparent bifurcation of the upper portion main BAM mineralisation to the west. The 3DM model has split the mineralisation domain into 2 separate domains. • To date there are no definitive interpreted major fault structures and dyke intrusives modelled from the logging data, but surface outcrop exposures show numerous dyke intrusives (tonalite and dolerite) and minor scale faulting. These structures are likely to have influence over grade continuity at a local scale.
Dimensions	• *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	• The Mineral Resource has an overall strike length of almost 3,000m with a maximum width of the mineralisation envelope being approximately 50m, down to minimum mining width of 3m. The main mineralisation zone within the BAM East toward BAM West area has a continuous strike length of over 1000m. • The Mineral resource is modelled to 380m vertical depth with the estimate based primarily on DD drilling collared from surface. The deepest hole to date has been drilled to approximately 384m depth (hole 0418-380). • A total of 21 mineralised domains were modelled for the January 2019 MRE. • There are minimal changes in strike and dip of the mineralisation across the sequence, and there is very good continuity overall from East to West for the main BAM mineralisation, but likely to be

Criteria	JORC Code explanation	Commentary
		affected by minor faulting and dolerite dyke intrusives, disrupting the mineralisation trends.
Estimation and modelling techniques	• *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.*	• Ordinary Kriging ("**OK**") estimation method was used to estimate gold into the 3D block model for the January 2019 MRE for the BAM Gold Project. • Samples were composited to 2m within each estimation domain, using fixed length option and a threshold inclusion of samples at sample length 50% of the targeted composite length. A 2m downhole composite was applied in order to reduce the variability inherent in raw samples or a smaller composite length relative to estimation resource model block dimensions. The 2m composite length is also closer to mining SMU for a large bulk mining open pit scenario. • Basic statistics were completed on all domains for the 2m composites, with the aim of evaluating the need for special treatment of obvious statistical outliers. Potential grade capping levels were determined using a combination of capping analysis tools (grade histograms, log probability plots and CVs). Grade capping was reviewed on a domain basis, where there was sufficient data. • Variogram modelling conducted to provide parameters for OK estimation method – nugget, sill and range for 3 directions. Variogram maps were initially analysed in plan, east-west and north-south section to confirm continuity trends and to refine parameters for experimental variogram calculation. Nugget values were calculated using downhole variograms. Variogram calculations were carried out on the 2m composites for all estimation domains. The variogram and search parameters for five well informed domains (were used to represent the poorly informed domains (smaller zones with very few composites). • The Kriging Neighbourhood Analysis ("**KNA**") function within Snowden's Supervisor software v8.8 ("**Supervisor**") software was used to assist with assessing the most appropriate block sizes and other estimation parameters such as minimum and maximum samples, discretisation, to be used for the estimation. • Parent block size of 25m x 10m x 10m in the X, Y, Z directions respectively was used and they were sub-blocked to 6.25m x 2.5m x 2.5m. • This was deemed to be appropriate for block estimation and modelling the selectivity for an open pit operation. • Au estimated in 3 passes – 1st pass using optimum search distances for each domain (max 100m) as determined through the KNA process, 2nd pass and 3rd pass used, set at longer distances in order to populate all blocks (2nd = max 200m, 3rd > 200m).
	• *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.*	• The current MRE estimate used ID^2 estimation as a check estimate against the OK estimation, with no significant variations in global estimate results for each projects. • The January 2019 MRE by Cube is an update of the December 2017 MRE produced and reported in accordance with NI 43-101 by RPA (RAP, 2018). The main changes from the RPA model include the re-interpretation of the main BAM mineralisation into a broader mineralised domain that can be selectively mined by open pit mining methods. Other changes included 2 m compositing instead of 1m composites, and the use of OK estimation method instead of ID^3 method adopted by RPA. Cube

Criteria	JORC Code explanation	Commentary
		also projected the mineralisation domaining out to the drilling fences to the east and west in order to identify potential drill target zones for step out a deeper drill testing in future. These zones were classified accordingly during the estimation process • There has been no previous mining activity at the BAM Gold Project and so there are no historical production records.
	• *The assumptions made regarding recovery of by-products.*	• No by-product recoveries were considered.
	• *Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).*	• Estimation of deleterious elements was not completed for the MRE. • The database contains mutli-element results for a broad suite of elements.
	• *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.*	• For all estimation domains, the first pass search radius selected was based on lode geometry and spatial data analysis.
	• *Any assumptions behind modelling of selective mining units.*	• The block model definition parameters included a primary block size and sub-blocking deemed appropriate for the mineralisation and to provide adequate volume definition where there are narrow or disrupted zones due to contacts or structural boundaries. • These dimensions are suitable for block estimation and modelling the selectivity for an open pit operation.
	• *Any assumptions about correlation between variables.*	• No correlation analysis between other elements and gold was conducted.
	• *Description of how the geological interpretation was used to control the resource estimates.*	• The mineralised domains acted as a hard boundary to control gold interpolation in the 2018 MRE block model. • The domaining was based on knowledge of the steeply mineralisation hosted within the BAM sequence known to host gold mineralisation from good quality diamond drilling information.
	• *Discussion of basis for using or not using grade cutting or capping.*	• After assessment of all domains, it was decided by Cube that no grade capping would be used for any of the domains as there was either no material difference when applying suitable top cut values, or there were no significant outliers for most of the domains. • Instead Cube has adopted the following method for dealing with high grade outliers: 1. No grade capping is applied to “extreme” Au values within the composite data for each domain; 2. Instead a cap (or “cut-off threshold”) them beyond a set distance away from the extreme sample is applied; 3. The spatial influence of these samples above the threshold is therefore limited to proximal blocks

Criteria	JORC Code explanation	Commentary
		(within a set distance) during grade estimation. • In all cases only a very small number of outlier values are included in the estimation domains that required cut-off threshold values to be applied.
	• *The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.*	• Block model validation was conducted by the following means: 1. Visual inspection of block model estimation in relation to raw drill data on a section by section basis. 2. Volumetric comparison of the wireframe/solid volume to that of the block model volume for each domain. 3. A global statistical comparisons of input and block grades, and local composite grade (by easting and RL) relationship plots (swath plots), to the block model estimated grade for each domain. 4. Comparison of the drill hole composites grades with the block model grades for each lode domain in 3D. • There are no historic workings and no recent mining activity has taken place at the BAM Gold Project, so there are mine reconciliation records.
Moisture	• *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	• The tonnages are estimated on a dry tonnes basis. Moisture was not considered in the density assignment.
Cut-off parameters	• *The basis of the adopted cut-off grade(s) or quality parameters applied.*	• The cut-off grade for reporting is 0.3g/t Au • As gold resources occur at near-surface the model was constructed with a view towards selective open pit mining and heap leach operation. Thus, a 0.3g/t Au lower cut-off was deemed appropriate.
Mining factors or assumptions	• *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.*	• Given the shallow nature of the mineralization and the initial metallurgical test results, material could be extracted by means of open pit mining methods and processed using conventional milling techniques. • 3DM modelling and block construction have been created with aim of preparing a suitable model for open pit mine design and pit optimisation, with a minimum mining width of 2m. Internal dilution has been considered with a maximum downhole width of 3m (2.5m true width) of sub-grade material (<0.2g/t Au). • The minimum block dimensions were selected based on a mining SMU of 6.25mE x 2.5mN x 2.5mRL. • An information effect was applied to the model and as such, the model was presented as a recoverable resource, implying that the practicalities of the mining operations are accounted for in the estimation process. As a result, Cube has not applied any further mining dilution or ore loss factors to the model.
Metallurgical factors or	• *The basis for assumptions or predictions*	• No metallurgical factors were considered during the interpretation and 3D modelling of the

Criteria	JORC Code explanation	Commentary
assumptions	*regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.*	mineralisation. • A series of metallurgical test programs have been carried out on samples from BAM East in 2017. • ALS Metallurgy Americas was engaged by LND in December 2016 to carry out a preliminary assessment of the metallurgical response of two composite samples from BAM East. The focus of the test program included an assessment for gold recovery through combined gravity concentration and cyanidation bottle roll leaching of the gravity tails at a single primary grind of 75 µm K80 (Sloan and Roulston, 2016). Between 98% and 99% of the feed gold was recovered through combined gravity concentration and cyanidation leaching of gravity tails for the two composites tested. Gold leach kinetics were fast, with most of the gold extraction taking place within the first six hours. Gold head grades were calculated at 2.0 g/t for both composites based on combined gravity and cyanidation leach test results (Sloan and Roulston, 2016). • LND completed additional metallurgical testing on the BAM East Gold Project in September of 2017 using samples collected from a drill hole completed in the summer 2017 drilling program (Sloan and Roulston, 2017). This additional test work was designed to assess the metallurgical response of two additional mineralized samples from the BAM East, and to provide a determination of the gold feed grade using gravity and cyanidation leach techniques, identical to those employed for the 2016 metallurgical test work. The metallurgical performance was excellent for both tested composites. Leach kinetics were rapid with most of the gold extraction completed within two to six hours, the combined gold recovery and cyanidation leach gold extractions for both composite samples measured between 97% to 99%, and the sodium cyanide and lime consumption was very low (<0.1 kg/tonne and 0.3 kg/tonne, respectively). Results indicate that a combination of gravity concentration followed by cyanidation leaching of the gravity tails would be an effective flowsheet for the composites tested.
Environmental factors or assumptions	• *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with*	• The Project area has previously been the subject of extensive ground disturbance as a result of forestry activities. • No assumptions were made regarding environmental restrictions.

Criteria	JORC Code explanation	Commentary
	an explanation of the environmental assumptions made.	
Bulk density	• *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.*	• The assigned bulk densities ("**BD**") are determined and based on samples taken by LND at the Junior Lake exploration camp. • BD measurements were taken where there was visible mineralization, and at 3m intervals in select holes for background measurements. • BD was measured utilizing a Denver Instrument Model PI-2002 scale, accurate to 0.01gm. The scale was securely setup on a sturdy table, and levelled. A plastic weighting basket was suspended beneath the scale so that it is completely submerged in a pail of water (at room temperature) and then the scale is calibrated to read zero. • The dry sample is weighted on the scale and the dry weight ("**DW**") recorded. The sample is then placed in the basket, completely submerged in the water and the wet weight ("**WW**") is recorded. • All dry and wet weights are entered into an MS Excel spreadsheet and the specific gravity is calculated using the following formula: • **BD=DW/DW-WW** • A total of 6,453 BD samples from 169 holes have been taken up to September 2018, representing 30% of all samples taken at BAM for analysis. The amount of BD samples is a good representation for all material types across the BAM Project area.
	• *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.*	• BD methodology is adequate for the rock material types at the BAM Project. There are no oxide/transition zones present within the sequence, and no porous or vuggy zones within the rock units below the shallow overburden material.
	• *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.*	• Cube also assigned assumed values for the overburden material (2.2t/m^3). • All lithology zones have been flagged with BD assigned values based on the interpreted lithological domains below the overburden surface: o BAM Sequence = 2.82 o Grassy Pond Sill = 2.84 o Marshall Lake Sequence = 2.9. • The assigned BDs are calculated averages for each lithology as reported by LND, based on database records collated from drilling and sampling up to September 2017.
Classification	• *The basis for the classification of the Mineral Resources into varying confidence categories.*	• Blocks have been classified as Indicated or Inferred based on data spacing and using a combination of kriging parameters and number of data used for the estimation: 1. Geological continuity and volume; 2. Drill spacing and drill data quality;

Criteria	JORC Code explanation	Commentary
		3. Modelling technique; 4. Estimation properties including search strategy, number of informing composites, average distance of composites from blocks and kriging quality parameters; and 5. Risk or uncertainty present in the estimated grades. • Indicated Mineral Resources are defined nominally by 50m x 50m spaced drilling or less. • Inferred Mineral Resources are defined by data greater than 50m x 50m spaced drilling and the confidence that the continuity of geology and mineralisation can be extended along strike and at depth to a nominal 50m maximum extent past Indicated Resource limit. • Unclassified material, all material within the mineralisation domains, but outside of indicated and inferred material – mostly Interpolation Pass 3 estimated material • The MRE appropriately reflects the Competent Person's view of the BAM Gold Project.
	• *Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).*	• The resource classifications are based on the quality of information for the geological domaining, as well as the drill spacing and geostatistical measures to provide confidence in the tonnage and grade estimates. • Drill holes oriented to the south, or drilled close to the same orientation as the mineralisation dip, were removed from the estimation composite data. There was sufficient confidence in all other data used, and the reliability of data based on high quality DD core.
	• *Whether the result appropriately reflects the Competent Person's view of the deposit.*	• The MRE appropriately reflects the Competent Person's view of the gold mineral resources.
Audits or reviews	• *The results of any audits or reviews of Mineral Resource estimates.*	• The estimation domaining, MRE parameters, classification and block model report replication have all been internally peer reviewed by qualified professionals at Cube.
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.*	• The January 2019 MRE is made up predominantly of broad to narrow, very continuous mineralised gold zones hosted within volcano-sedimentary sequence. • The current modelled MRE is a reasonable representation of the global contained metal. • The resource risk is considered to be low to moderate. • The density of drilling supports the classification of 74% of the Mineral Resource to be classified as Indicated (by contained metal). • Recent infill DD drilling has verified the reproducibility of the original mineralised drill intersections from the early stages of drilling. • Whilst QAQC analysis completed so far for the recent drilling in 2018 is satisfactory, recommendations have been included in Table 1 in order to follow up precision and bias related to duplicate sampling and check sampling by an independent laboratory.
	• *The statement should specify whether it relates to global or local estimates, and, if*	• The MRE constitutes a global resource estimate.

Criteria	JORC Code explanation	Commentary
	local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.	
	• *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	• No previous mining activity has taken place with the Project area.

Appendix A – 2018 Drilling Information for BAM Gold Project

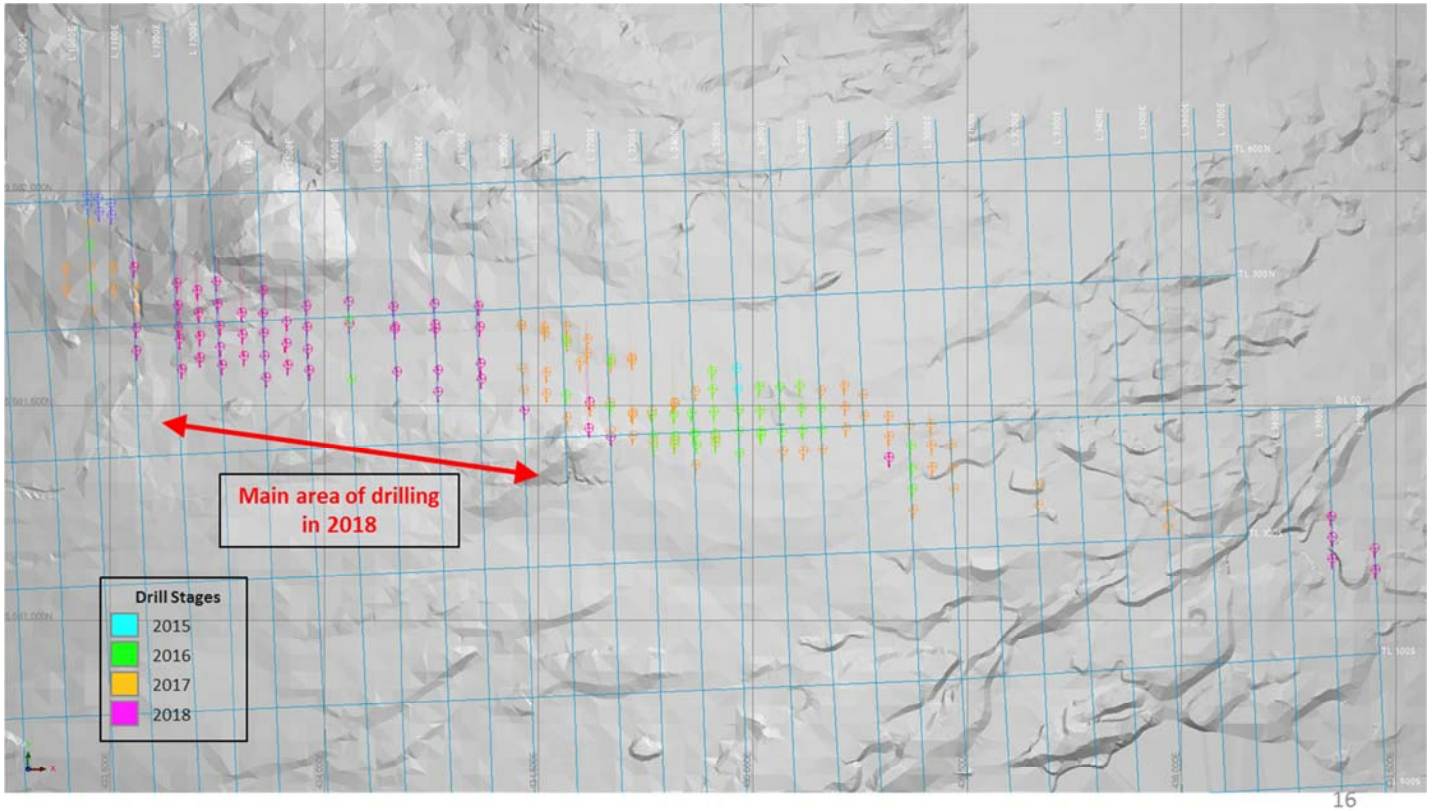
Hole ID	utm z16_n83 easting	utm z16_n83 northing	Elevation (m)	Hole Depth (m)	Hole Size	local grid easting	local grid northing	Plan_Azi	Plan_Dip		Depth From (m)	Interval Length (m)	Grade (g/t Au)
0418-626	433,553.79	5,581,822.88	363.50	206.77	NQ	1100	450	357	-45				
0418-627	433,558.73	5,581,682.59	357.80	263.03	NQ	1100	300	357	-45		209.04	3.81	1.94
0418-628	433,654.06	5,581,785.82	372.91	108.50	NQ	1200	400	357	-45		22.53	**41.27**	1.10
										including	44.24	7.61	3.10
										and	62.80	1.00	**11.70**
0418-629	433,656.17	5,581,734.82	368.90	177.08	NQ	1200	350	357	-45		120.21	**16.10**	1.16
0418-630	433,745.71	5,581,790.13	370.60	105.00	NQ	1300	400	357	-45		21.00	17.65	0.71
0418-631	433,749.00	5,581,739.21	362.98	159.10	NQ	1300	350	357	-45		13.12	0.72	**24.90**
										and	74.02	0.70	4.26
										and	83.00	**15.80**	1.01
										including	89.45	5.00	2.29
0418-633	433,854.34	5,581,769.31	365.70	114.00	NQ	1400	375	357	-45		108.57	2.43	3.99
0418-634	433,854.98	5,581,716.25	357.41	180.05	NQ	1400	325	357	-45		84.50	10.58	2.03
										including	90.47	1.00	**16.15**
0418-635	433,955.57	5,581,733.83	355.97	122.97	NQ	1500	340	357	-45		57.40	5.55	1.55
0418-636	433,957.45	5,581,684.73	353.72	168.06	NQ	1500	290	357	-45		128.51	3.72	1.63
0418-637	434,054.58	5,581,744.59	354.60	111.00	NQ	1600	340	357	-45		49.77	4.87	1.41
0418-638	434,056.10	5,581,692.87	352.11	221.85	NQ	1600	290	357	-60				
0418-639	434,159.44	5,581,732.73	354.80	134.94	NQ	1700	325	357	-45		60.78	5.62	0.95
0418-640	434,162.43	5,581,683.80	352.99	152.89	NQ	1700	275	357	-45				
0418-641	434,162.90	5,581,679.57	352.99	197.81	NQ	1700	270	357	-60				
0418-642	434,254.77	5,581,739.14	355.00	89.99	NQ	1800	325	357	-45				
0418-643	434,256.65	5,581,691.19	353.00	135.05	NQ	1800	275	357	-45				

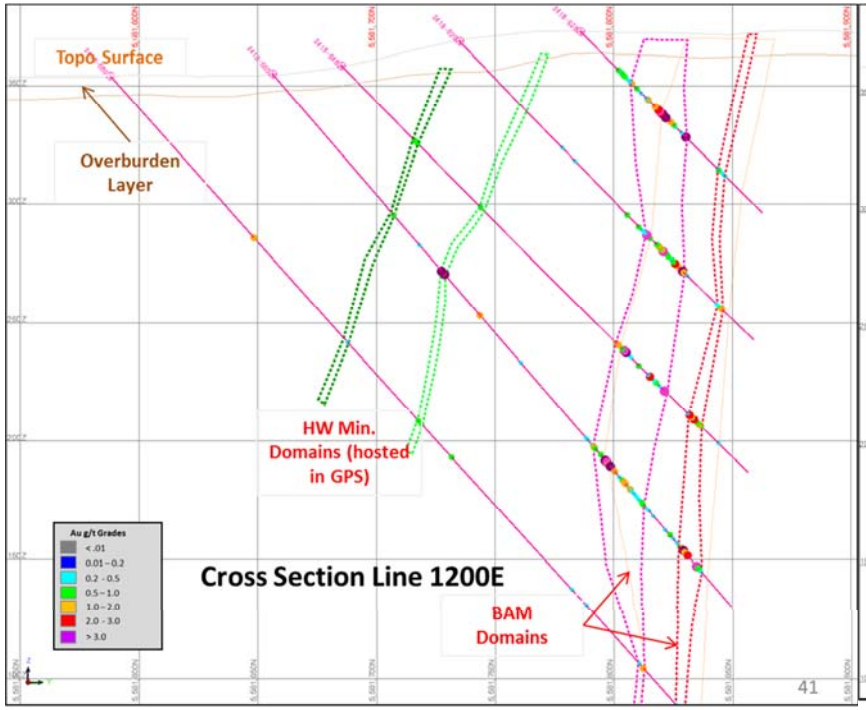
Hole ID	utm z16_n83 easting	utm z16_n83 northing	Elevation (m)	Hole Depth (m)	Hole Size	local grid easting	local grid northing	Plan_Azi	Plan_Dip		Depth From (m)	Interval Length (m)	Grade (g/t Au)
0418-644	434,258.24	5,581,680.14	353.00	183.02	NQ	1800	265	357	-55				
0418-645	434,357.85	5,581,734.26	354.30	120.04	NQ	1900	315	357	-45				
0418-646	434,360.75	5,581,684.53	352.60	113.84	NQ	1900	265	357	-45				
0418-647	433,856.81	5,581,670.36	353.51	203.64	NQ	1400	275	357	-45		133.12	12.82	1.12
0418-648	433,657.33	5,581,684.98	358.77	242.95	NQ	1200	300	357	-45		164.88	6.33	1.88
										and	184.52	9.63	0.93
										and	208.05	7.55	1.17
0418-649	434,667.55	5,581,427.63	354.66	333.00	HQ	2200	0	357	-50				
0418-650	434,618.04	5,581,510.28	351.94	243.04	HQ	2150	85	357	-40				
0418-651	434,616.25	5,581,448.78	356.47	311.86	HQ	2150	20	357	-45				
0418-652	434,465.21	5,581,490.58	354.13	305.93	HQ	2000	70	357	-45				
0418-656	434,363.10	5,581,599.80	352.43	204.34	HQ	1900	185	357	-40				
0418-657	434,364.50	5,581,563.90	352.43	246.00	HQ	1900	150	357	-45				
0418-658	434,263.30	5,581,584.70	352.43	242.98	HQ	1800	175	357	-45				
0418-659	434,263.80	5,581,533.20	352.43	299.97	HQ	1800	125	357	-45				
0418-660	434,167.20	5,581,582.00	352.32	269.86	HQ	1700	170	357	-48				
0418-661	433,963.40	5,581,584.90	352.78	294.06	HQ	1500	190	357	-45		227.35	**34.49**	0.80
										including	235.35	10.12	1.46
0418-662	433,960.00	5,581,633.60	352.72	218.99	HQ	1500	240	357	-45				
0418-663	433,859.30	5,581,618.20	353.51	272.99	HQ	1400	225	357	-45		210.29	5.63	1.70
										and	232.11	11.95	2.17
0418-664	433,755.10	5,581,638.50	355.26	270.02	HQ	1300	250	357	-45		194.10	**31.24**	1.30
0418-665	433,660.30	5,581,656.10	355.11	296.91	HQ	1200	275	357	-50		109.06	2.94	**11.84**
										including	111.00	1.00	**28.80**
										and	207.46	**32.89**	1.03

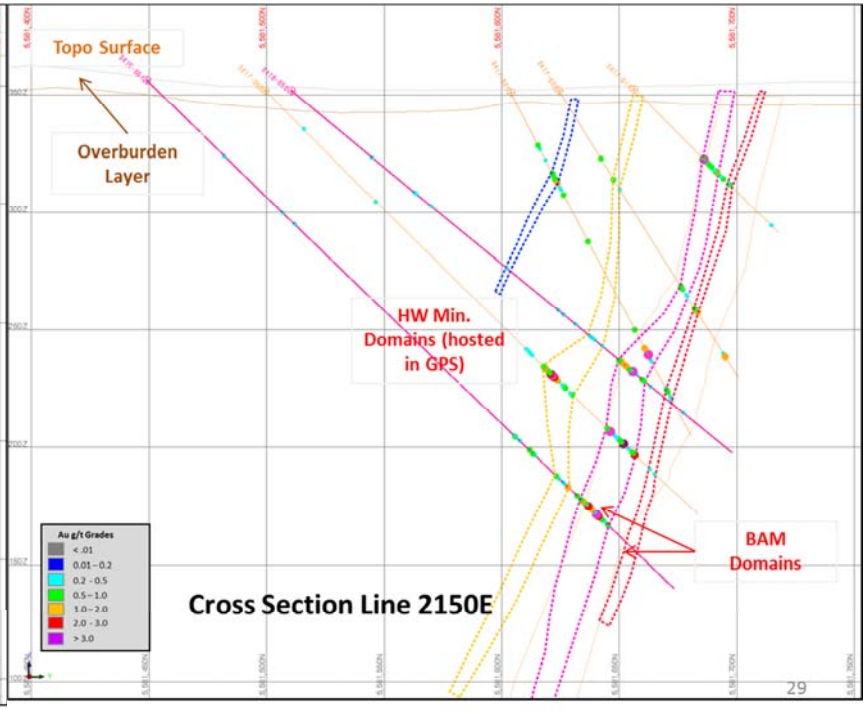
Hole ID	utm z16_n83 easting	utm z16_n83 northing	Elevation (m)	Hole Depth (m)	Hole Size	local grid easting	local grid northing	Plan_Azi	Plan_Dip		Depth From (m)	Interval Length (m)	Grade (g/t Au)
										including	214.88	4.00	5.30
										and	264.15	5.00	2.65
0418-666	433,560.00	5,581,630.30	353.92	333.01	HQ	1100	250	357	-45		117.95	0.80	**12.10**
										and	288.95	4.15	3.36
0418-667	433,910.40	5,581,697.50	353.72	165.08	HQ	1450	300	357	-45				
0418-668	433,909.70	5,581,646.60	352.95	213.05	HQ	1450	250	357	-45				
0418-669	433,912.60	5,581,597.20	352.89	284.71	HQ	1450	200	357	-45		222.00	17.55	0.72
										and	250.50	6.97	2.56
										including	254.90	1.10	8.00
0418-670	433,805.70	5,581,717.50	359.87	170.62	HQ	1350	325	357	-45				
0418-671	433,806.90	5,581,667.90	354.21	233.94	HQ	1350	275	357	-45		55.12	1.00	**11.95**
										and	159.27	15.61	1.43
										and	194.40	10.71	1.77
										including	194.40	0.82	**10.20**
0418-672	433,810.50	5,581,617.30	353.51	284.94	HQ	1350	225	357	-45		234.74	9.46	0.79
										and	256.22	4.40	5.29
0418-673	433,701.70	5,581,769.30	370.70	126.07	HQ	1250	375	357	-45				
0418-674	433,705.00	5,581,718.10	362.25	180.00	HQ	1250	325	357	-45				
0418-675	433,707.40	5,581,663.30	357.10	263.84	HQ	1250	275	357	-45		190.00	**21.07**	1.47
										including	190.00	1.00	**12.45**
0418-676	433,754.50	5,581,687.40	358.37	225.00	HQ	1300	297	357	-45		144.30	12.60	1.41
										including	150.70	1.00	**9.59**
										and	170.43	4.12	1.83
0418-677	433,708.10	5,581,614.40	355.58	320.95	HQ	1250	225	357	-45				
0418-678	433,759.30	5,581,597.00	353.65	333.05	HQ	1300	200	357	-47				

Hole ID	utm z16_n83 easting	utm z16_n83 northing	Elevation (m)	Hole Depth (m)	Hole Size	local grid easting	local grid northing	Plan_Azi	Plan_Dip		Depth From (m)	Interval Length (m)	Grade (g/t Au)
0418-679	433,862.10	5,581,567.30	353.50	348.00	HQ	1400	175	357	-47		313.27	1.25	**32.00**
0418-680	433,665.10	5,581,587.60	354.51	383.95	HQ	1200	200	357	-48				
0418-681	436,347.90	5,581,597.00	342.06	50.90	HQ	3900	-250	357	-45				
0418-682	436,350.30	5,581,195.80	340.66	99.07	HQ	3900	-300	357	-45		65.00	1.00	1.84
0418-683	436,350.90	5,581,145.80	340.91	152.98	HQ	3900	-350	357	-45				
0418-684	436,449.80	5,581,170.80	342.42	62.92	HQ	4000	-325	357	-45				
0418-685	436,451.60	5,581,120.80	342.51	116.90	HQ	4000	-375	357	-45		77.00	1.02	**26.20**
										and	86.00	1.00	1.14
0418-686	435,317.10	5,581,379.90	351.97	162.02	HQ	2850	-75	357	-45		133.02	0.51	**14.95**

Appendix B – Drill Plan and a Representative Drill Sections (1200E and 2150E)




Topo Surface
Overburden Layer
HW Min. Domains (hosted in GPS)
BAM Domains
Cross Section Line 1200E
Au g/t Grades
< .01
0.01 – 0.2
0.2 - 0.5
0.5 – 1.0
1.0 – 2.0
2.0 - 3.0
> 3.0
41


Topo Surface
Overburden Layer
HW Min. Domains (hosted in GPS)
BAM Domains
Cross Section Line 2150E
Au g/t Grades
< .01
0.01 – 0.2
0.2 - 0.5
0.5 – 1.0
1.0 – 2.0
2.0 - 3.0
> 3.0
29

Appendix C – Potential Extensions to Mineralisation at BAM Gold Project